



TR-0310

AD-A251 892



AD

Reports Control Symbol
OSD - 1366

2

COMPUTATION OF INFRARED TRANSMITTANCES
IN THE TROPOSPHERE USING SATELLITE VALUES
OF PRECIPITABLE WATER: PRELIMINARY METHOD

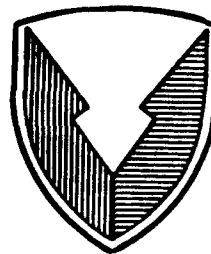
May 1992

James Cogan

DTIC
ELECTE
JUN 22 1992
S B D

92 6 19 024

Approved for public release; distribution is unlimited.



US ARMY
LABORATORY COMMAND

92-16311



ATMOSPHERIC SCIENCES LABORATORY
White Sands Missile Range, NM 88002-5501

NOTICES

Disclaimers

The findings in this report are not to be construed as an official Department of the Army position, unless so designated by other authorized documents.

The citation of trade names and names of manufacturers in this report is not to be construed as official Government indorsement or approval of commercial products or services referenced herein.

Destruction Notice

When this document is no longer needed, destroy it by any method that will prevent disclosure of its contents or reconstruction of the document.

REPORT DOCUMENTATION PAGE			Form Approved OMB No. 0704-0188	
Public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Washington Headquarters Services, Directorate for Information Operations and Reports, 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA 22202-4302, and to the Office of Management and Budget, Paperwork Reduction Project (0704-0188), Washington, DC 20503.				
1. AGENCY USE ONLY (Leave blank)	2. REPORT DATE May 1992	3. REPORT TYPE AND DATES COVERED Final		
4. TITLE AND SUBTITLE Computation of Infrared Transmittances in the Troposphere Using Satellite Values of Precipitable Water: Preliminary Method		5. FUNDING NUMBERS DA Task # 62784/AH71/D		
6. AUTHOR(S) James Cogan				
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) U.S. Army Atmospheric Sciences Laboratory White Sands Missile Range, NM 88002-5501		8. PERFORMING ORGANIZATION REPORT NUMBER ASL-TR-0310		
9. SPONSORING / MONITORING AGENCY NAME(S) AND ADDRESS(ES) U.S. Army Laboratory Command Adelphi, MD 20783-1145		10. SPONSORING / MONITORING AGENCY REPORT NUMBER		
11. SUPPLEMENTARY NOTES				
12a. DISTRIBUTION / AVAILABILITY STATEMENT Approved for public release; distribution is unlimited.		12b. DISTRIBUTION CODE		
13. ABSTRACT (Maximum 200 words) Transmittance in the thermal infrared may be estimated from various in situ and remote techniques using ground-based or airborne sensors. However, estimating transmittance in the troposphere from data gathered by sensors on space platforms remains a problem, especially over land surfaces. This report presents a preliminary method for computing thermal infrared transmittance over a horizontal, vertical, or slant path. This method uses estimates of precipitable water from satellite data combined with sounding data from satellite or other sources. A brief description of the technique and a brief sensitivity analysis provide a basic understanding of the method. Profiles of specific humidity are computed from actual atmospheric profiles or climatological data and then adjusted according to satellite estimates of total precipitable water. Temperature and humidity data at each pressure level provide input to equations of the types found in LOWTRAN. These equations yield estimates of thermal infrared transmittance for user-specified path lengths.				
14. SUBJECT TERMS infrared transmittance, satellite data, transmittance model, satellite meteorology		15. NUMBER OF PAGES 18		
		16. PRICE CODE		
17. SECURITY CLASSIFICATION OF REPORT Unclassified	18. SECURITY CLASSIFICATION OF THIS PAGE Unclassified	19. SECURITY CLASSIFICATION OF ABSTRACT Unclassified	20. LIMITATION OF ABSTRACT SAR	

CONTENTS

LIST OF ILLUSTRATIONS	4
1. INTRODUCTION	5
2. DESCRIPTION OF METHOD	5
2.1 Overview	5
2.2 Transmittance Algorithms	6
2.3 Precipitable Water Adjustment	8
3. COMPARISONS AND SIMULATIONS	9
3.1 Comparisons	9
3.2 Modified Method	10
3.3 Simulations	10
4. CONCLUSION	11
LITERATURE CITED	17
DISTRIBUTION LIST	19



Accession For	
NTIS GRA&I	<input checked="" type="checkbox"/>
DTIC TAB	<input type="checkbox"/>
Unannounced	<input type="checkbox"/>
Justification	
By _____	
Distribution/	
Availability Codes	
Dist	Avail and/or Special
A-1	

LIST OF ILLUSTRATIONS

Table 1. Results from Transmittance Computations Using LOWTRAN 7 (L) and the approximate Method (A).....	12
Table 2. Transmittance Results Using GENLN2 (G), LOWTRAN 7 (L), and the Approximate Method (A)	12
Table 3. Transmittance Computed for AVHRR Channels 4 and 5 for Three Model Atmospheres	13
Table 4. Transmittance Computed for AVHRR Channels 4 and 5 for Important Absorbers/Scatterers	13
Table 5. Transmittances Computed with the Approximate Method Using the Mid-Latitude Summer Atmosphere	14
Figure 1. Transmittance (τ) values for channel 5 computed using the approximate method for the mid-latitude summer atmosphere for 3 km horizontal paths at the indicated heights (Z) for the listed values of PW in g cm^{-2}	15
Figure 2. Transmittance (τ) values for channel 5 computed using the approximate method for the subarctic winter atmosphere for 3 km horizontal paths at the indicated heights (Z) for the listed values of PW in g cm^{-2}	15
Figure 3. Transmittance (τ) values for channel 5 computed using the approximate method for the tropical atmosphere for 3 km horizontal paths at the indicated heights (Z) for the listed values of PW in g cm^{-2}	16
Figure 4. Transmittance (τ) values for channel 5 computed using the approximate method for an actual sounding for 3 km horizontal paths at the indicated heights (Z) for the listed values of PW in g cm^{-2}	16

1. INTRODUCTION

Determining atmospheric infrared transmittance in the troposphere is a major problem for remote or denied areas. Air or space-based platforms may carry in situ devices or remote sensing instruments. However, methods to estimate infrared transmittance by using data from space platforms remain a problem, especially over land surfaces. This report presents a preliminary method to compute thermal infrared transmittance over a horizontal, vertical, or slant path. The method uses estimates of precipitable water from satellite data combined with sounding data from satellite or other sources. If sounding data are unavailable, or too distant in space or time from the area or time of interest, then climatological profile data may be used to provide an approximate estimate. A brief description of the technique and a brief sensitivity analysis provide a basic understanding of the method. Profiles of specific humidity are computed from actual atmospheric profiles or climatological data and then adjusted according to satellite estimates of total precipitable water.

2. DESCRIPTION OF METHOD

2.1 Overview

The preliminary technique uses the relation between water vapor and infrared extinction in the atmosphere. Algorithms of the types found in LOWTRAN (low resolution transmittance and radiance) may be used to compute infrared transmittance in a horizontally stratified atmosphere (Kneizys et al., 1980, 1983, 1988). Temperature and humidity data at each pressure level of an atmospheric sounding provide input to equations similar to those found in Kneizys et al. (1980). The older version of LOWTRAN used standard type variables (for example, vapor pressure in atmospheres). The accuracy in the thermal infrared is virtually the same as in Kneizys et al. (1983), and the algorithms are the same in Kneizys et al. (1988) and Kneizys et al. (1983). These equations yield estimates of thermal infrared transmittance for user-specified horizontal, vertical, or slant path lengths. The preliminary version assumes a horizontally homogeneous layer at a given pressure (that is, horizontally stratified atmosphere). The simple integration techniques of this approximate method assume constant or only slowly varying transmittance over spectral intervals of up to 20 cm^{-1} . Nominally this method can give results for smaller spectral intervals (to 1 cm^{-1}). However, for this investigation 20 cm^{-1} intervals were used and did not appear to degrade the results in this case.

Generally, atmospheric soundings from various sources may be used, but for applications to remote areas the primary sources would be satellite soundings, soundings derived from aircraft or unmanned aerial vehicle (UAV) data, dropsonde profiles, or a combination of the above (Cogan, 1990). The resultant sounding provides temperature (T) and humidity (h) values at given pressure levels, which may be used to compute specific humidity (q). From values of q one may compute precipitable water (PW) for layers or for the entire vertical extent of the sounding (total or integrated PW). Integrated values of PW may be compared to values derived from satellite imagery. The sounding amount (not the shape of the distribution curve) is adjusted according to the ratio of the estimate from satellite imagery (called satellite estimate or value in this report) to the

value computed from the sounding. If sounding data are not available for the time and area of interest, then climatological profiles for the most appropriate region and season may be used. The accuracy most likely will degrade, but useful gradient information may be possible.

Several investigators using, for example, transmittance ratios (total through entire atmosphere) have developed techniques for satellite estimates of PW. Chesters et al. (1983) and Chesters et al. (1987) used split window radiances from the Visible Infrared Spin Scan Radiometer (VISSR) Atmospheric Sounder (VAS) carried on Geostationary Operational Environmental Satellites (GOES). Jedlovec (1989) and Kleespies and McMillin (1990) developed methods that used data from both the VAS and the Advanced Very High Resolution Radiometer (AVHRR) carried by National Oceanographic and Atmospheric Administration (NOAA) satellites. Jedlovec (1989) derived his method by using aircraft data and then applied it to satellite values. Kleespies and McMillin (1990) reported correlations as high as 0.85 (AVHRR) and 0.92 (VAS) relative to PW from radiosonde data. Ongoing work in this area could lead to improved absolute accuracies.

2.2 Transmittance Algorithms

The author assumed that atmospheric soundings provide profiles of T (K), h (%), and z (m) at several pressure levels. Pressure (p) has units of hPa (= mbar). Values of h are converted to values of absolute humidity q (g m^{-3}) through the standard equations found in references such as Ludlam (1980). First, saturation vapor pressure (e_s) in hPa is computed.

$$e_s = 6.108 \exp(17.27(T - 273.16)/(T - 35.86)) \quad (1)$$

Then e_s is used in the computation of q by the formula:

$$q = (e(10^6)/TR_v)h/100, \quad (2)$$

where R_v is the gas constant for water vapor. Climatological profiles may include values of q , in which case the above equations are not required. From the q profile, PW for each layer (i) in units of g cm^{-2} is computed from

$$(PW)_i = 0.1(z_{i+1} - z_i)(q_{i+1} + q_i)/2. \quad (3)$$

The layer values of PW are summed to get the total PW. The ratio of the satellite-measured value of PW to the total PW from the sounding is used to scale the values of q for each pressure level or height.

The resultant profile of q is used with equations of the types found in Kneizys et al. (1980) for computing transmittance for the mean wave number of a narrow

spectral interval. First, however, e (in units of atm) is computed using a variation of equation (2).

$$e = qTR_v(10^{-6})/p_0,$$

where p_0 is standard pressure (= 1013.25 hPa). A LOWTRAN water vapor parameter (w) (the effective water vapor absorber amount per unit path length in $\text{g cm}^{-2} \text{ atm km}^{-1}$ at altitude z) is computed using the following:

$$w = 0.1q[e(\exp[6.08(296/T - 1)]) + 0.002(p - e)], \quad (4)$$

where p is in units of atm. The water vapor attenuation coefficient (C_s) in $\text{g}^{-1} \text{ cm}^2 \text{ atm}^{-1}$ (\approx absorption in the thermal infrared), as defined in Kneizys et al. (1980) for a thermal infrared wave number (ν) in the 8 to 14 μm wavelength region at a temperature of 296 K, is given by

$$C_s = 4.18 + 5578 \exp(-0.00787\nu). \quad (5)$$

Finally, the transmittance (τ) for a given thermal infrared wave number is computed from a variation of the standard equation

$$\tau = \exp(-C_s w D_s). \quad (6)$$

This procedure should be valid for a narrow wave number band in the thermal infrared to a useful accuracy. For example, τ for the mean wave number of a 20-cm^{-1} band, as used in LOWTRAN, provides a reasonable estimate of τ for that interval. The assumption is that transmittance is constant or only varies slowly and fairly smoothly over a 20-cm^{-1} interval. However, the use of LOWTRAN to compute monochromatic transmittances (as for a laser) may lead to serious errors (McClatchey et al., 1972). The same warning also applies to the method this author devised, which was derived from LOWTRAN.

The equations for carbon dioxide, ozone, and noncontinuum water vapor were derived from LOWTRAN equations for "uniformly mixed gases" (for example, carbon dioxide) and water vapor (Kneizys et al., 1980). Transmittance over an interval of 20 cm^{-1} is computed from an equation of the form $\tau = f(C_n w^* D_s)$, where C_n is a wave number dependent absorption coefficient, w^* is an equivalent absorber density, and D_s is the atmospheric path.

$$w^* = w \left[\frac{p(z)}{p_0} \sqrt{\frac{T_0}{T(z)}} \right]^m \quad (7)$$

where p_0 and T_0 correspond to standard pressure and temperature (1 atm = 1013.25 hPa, 273.16 K). m has values of 0.9, 0.75, and 0.4 for water vapor, carbon dioxide, and ozone, respectively. In LOWTRAN the form of the function for τ and the parameter m were determined empirically using laboratory transmittance data and molecular line constants (Kneizys et al., 1980). Curves were computed based on these data and presented in Kneizys et al. (1980) for τ (graphed as log to the base 10 of τ), C_n , and absorber concentrations. The curve of $\log_{10} \tau$ for ozone is different from that for water vapor (noncontinuum) and the uniform mixed gases, but the basic form is similar. The units for the C_n and concentrations differed, but can be converted to "standard" units through the use of relationships given in McClatchey et al. (1972).

The approach for aerosols was based on the technique of Kneizys et al. (1980). This preliminary report considers only distributions for land aerosols (rural and urban). Later, Kneizys et al. (1983) improved the distribution for the lowest 2 km over land by using routines based on Heaps (1982). More recent updates as noted in Kneizys et al. (1988) should improve matters further, but no documentation existed when this report was prepared. However, the earlier approach should be sufficiently accurate for the research described in this report.

Kneizys et al. (1980) presented profiles of aerosols for various situations, including the rural and urban curves, maritime distributions, and curves for after volcanic eruptions. Seasonal and high humidity differences were included. However, for the preliminary effort described here, mean curves for the basic profiles for land, rural and urban, were thought to be sufficient. Transmittance was then calculated through an equation of the form $\tau(\text{aerosol}) = \exp(-\text{extinction coef} * \text{haze scale factor value} * \text{distance})$.

In the program of this report the aforementioned curves were approximated through piecewise linear or power law fits, or a combination of both. Other fits may produce a closer approximation, but the ones chosen gave a sufficiently good fit for this initial investigation.

2.3 Precipitable Water Adjustment

PW is calculated from q for layers determined by the sounding levels, and then summed to obtain a total integrated value for the sounding (PW_s). Values of PW may be calculated from satellite imagery (PW_i) by a method such as the methods developed by Chesters et al. (1983), Chesters et al. (1987), Jedlovac (1989), and Kleespies and McMillin (1990). Each layer value of q (q linearly related to PW) is then multiplied by the ratio PW_i/PW_s . The adjusted layer values of q are used in computing τ by the method described above. If more than one sounding is close to a particular location, then appropriate mean values for computing the ratio should be used. However, such a procedure had not been incorporated in this preliminary technique.

3. COMPARISONS AND SIMULATIONS

3.1 Comparisons

The approximate method of this report for computing thermal infrared transmittances was compared with LOWTRAN 7 (PC version) for vertical paths from the surface to 14 km. In particular the spectral intervals covered by channels 4 and 5 of the AVHRR were chosen for the comparison (885-971 and 800-870 cm^{-1}). For this comparison the spectral responses of the actual instrument were not considered (that is, step function response used), and a rural aerosol with a 23-km visibility was assumed.

As noted above, the calculations of this report did not account for sensor response as did those for the GENLN2. However, sample computations with the U. S. standard and tropical atmospheres suggested that leaving out the response function (that is, assuming constant response across the interval) only led to relatively small errors in results from the approximate method of this report and LOWTRAN. The errors were < 0.002 for channel 4 and ≤ 0.01 for channel 5. All values that were computed with the sensor response included were higher, and magnitudes were larger for the tropical atmosphere. Nevertheless, the closeness of the approximate method and GENLN2 results, with the possible "errors" considered, may be fortuitous. However, the method apparently can produce useful results for a cloud free line of sight.

Table 1* shows the results of the comparison for a few of the "standard" atmospheres. The differences in τ were small to moderate except for the much larger difference (over 0.06) for the subarctic winter atmosphere. Transmittances from both LOWTRAN and the program of this report were compared to those from a line-by-line method (GENLN2) as reported by Saunders and Edwards (1989). Table 2 compares values of τ computed over a vertical path from 0 to 100 km for the U.S. standard atmosphere with an urban aerosol by the approximation program of this report, the PC version of LOWTRAN 7, and the GENLN2 line-by-line program. The GENLN2 values are listed as presented in Saunders and Edwards, that is, rounded to the nearest 0.01.

Neither LOWTRAN nor the approximate method produced values equal to the GENLN2 results, but nearly all the approximation values were closer. A comparison of the results shown in table 1 with those derived from data presented in Saunders and Edwards (1989) suggested that, except for the tropical atmosphere, the approximation values were closer to the GENLN2 output (especially for the subarctic winter case). In all cases the line-by-line calculations led to higher values of τ than either of the lower resolution programs. However, different line-by-line models may not yield the same values. Saunders and Edwards noted that Chedin et al. (1988) reported that for nadir paths in the 15- μm region various transmittance models only agree to within 2 percent in τ .

*Tables and figures are presented at the end of the text.

3.2 Modified Method

The approximate method was analyzed and compared to the line-by-line model for several atmospheric constituents. The main differences from the line-by-line results were for water vapor, especially continuum absorption. The differences were nonlinear, and they increased with increasing water vapor amount. A minor change to the wave number coefficient in equation (5) from -0.00787 to -0.00817 resulted in significantly closer values for the more moist atmospheres, especially for the tropical case. Table 3 shows some results of the comparison between the GENLN2 and modified approximate method. For channel 5 (800-870 cm^{-1}) the two sets of values agreed to within 0.004, and for channel 4 (885-971 cm^{-1}) the largest difference was 0.011. Both maximum differences were computed for the subarctic winter atmosphere. The values presented in table 3 may be compared with LOWTRAN 7 and unmodified approximate results in table 1.

Saunders and Edwards (1989) published results by absorber/scatterer for the U. S. standard atmosphere that were compared to those computed by the modified method. As seen in table 4 the two methods produced values that agree reasonably well. Certain of the Saunders and Edwards results were presented to the nearest 0.01 and others to 0.0001; the former values are shown as printed and the latter are rounded to the nearest 0.001, as was the output from the approximate method. The maximum difference apparently did not exceed about 0.01, and would have been smaller if the response curves had been used.

3.3 Simulations

Various simulations were made with the approximate method to get an idea of the likely errors in τ that would be associated with typical errors in PW from satellite data. Chesters et al. (1983) reported an overall rms error in total PW computed from VAS data of about $\pm 1.0 \text{ g cm}^{-2}$ over a range of PW values from 1.7 to 5.5 g cm^{-2} . In a later paper by Chesters et al. (1987) the error was reduced to $\pm 0.6 \text{ g cm}^{-2}$. Kleespies and McMillin (1990) found a standard difference of around 0.44 g cm^{-2} when their technique was applied to AVHRR data, and 0.39 g cm^{-2} for VAS data. For all of the above methods, single comparisons with data from individual rawinsondes gave differences of up to around 2 or 3 g cm^{-2} . For this report τ values were calculated for the tropical and mid-latitude summer atmospheres where the total PW was changed by ± 0.5 and $\pm 1.0 \text{ g cm}^{-2}$. The results of those computations for the mid-latitude summer are shown in table 5. Figure 1 shows the variation of τ for horizontal paths of 3 km at each level up to 6 km for channel 5 for the same model atmosphere with a PW variation of $\pm 0.5 \text{ g cm}^{-2}$. As indicated in the figure the differences in horizontal τ at lower levels can be significant for the given "errors" in PW.

Figures 2 and 3 present curves similar to those of figure 1 for the subarctic winter and tropical atmospheres. The curve in figure 2 for $\text{PW} = 0.000 \text{ g cm}^{-2}$ shows τ values for a completely dry atmosphere. Among the standard atmospheres the greatest change in τ for a change in PW of $\pm 0.5 \text{ g cm}^{-2}$ apparently occurred for the fairly moist ($\text{PW} = 2.977 \text{ g cm}^{-2}$) mid-latitude summer atmosphere. A slightly smaller change occurred for the less moist ($\text{PW} = 1.448 \text{ g cm}^{-2}$) U.S. standard atmosphere (not shown). Figure 4 was calculated for a real rawinsonde sounding launched about 16 Z on 26 September 1980 at Dayton, Ohio (Bradford et al., 1982). A fairly strong subsidence inversion capped a modestly moist layer

below 2 km. The values of τ below 2 km exhibit changes greater than those shown by any of the standard atmospheres of figures 1 through 3 and the U. S. standard atmosphere when PW is varied by $\pm 0.5 \text{ g cm}^{-2}$. This very limited comparison with real data supports the idea that use of climatological data to estimate τ would lead to less accurate results and that actual sounding data should be used whenever possible.

4. CONCLUSION

A preliminary technique was developed for estimating transmittance in the thermal infrared in the troposphere by using satellite-derived values of PW along with profile data that are not too distant in space or time. The computer model was written in the "C" computer language and can run on an 80286-based computer (with math coprocessor) in a few seconds. Furthermore, Chesters et al. (1983) noted that relative accuracies are very good compared to absolute accuracies. Consequently, adjusting a coincident satellite-derived value of PW to that extracted from the profile data may allow a useful description of the surrounding moisture field.

The apparent accuracy of the approximate method for computing τ of about 0.01 relative to a line-by-line model seems reasonably useful for many cloud free atmospheres. Present plans include a further comparison with the very recent version of MODTRAN (moderate resolution transmittance and radiance) that can run on an 80386-based computer (with math coprocessor) and real transmittance data (when available) to further refine the method. However, the primary source of error appears to arise from the satellite estimates of PW. An error in PW of $\pm 0.5 \text{ g cm}^{-2}$ can lead to errors in τ for a 3-km horizontal path that may exceed 0.10 (figure 4). Therefore, further work will concentrate more on improving the technique for estimating PW from satellite imagery.

TABLE 1. RESULTS FROM TRANSMITTANCE COMPUTATIONS USING
LOWTRAN 7 (L) AND THE APPROXIMATE METHOD (A)*

Atmosphere	Model	Transmittance	
		ch 4	ch 5
<i>Tropical</i>	<i>L</i>	0.516	0.368
	<i>A</i>	0.509	0.363
<i>Mid Latitude Summer</i>	<i>L</i>	0.641	0.522
	<i>A</i>	0.662	0.541
<i>Subarctic Winter</i>	<i>L</i>	0.870	0.850
	<i>A</i>	0.941	0.927

*The PC version of LOWTRAN was used.

TABLE 2. TRANSMITTANCE RESULTS USING
GENLN2 (G), LOWTRAN 7 (L)
AND THE APPROXIMATE METHOD (A)*

Model	Transmittance	
	ch 4	ch 5
<i>G</i>	0.85	0.80
<i>L</i>	0.792	0.737
<i>A</i>	0.851	0.792

*The results from GENLN2 (a line-by-line model)
were presented in Saunders and Edwards (1989).
All results were for the U.S. standard atmosphere.

TABLE 3. TRANSMITTANCE COMPUTED FOR AVHRR CHANNELS 4 AND 5 FOR THREE MODEL ATMOSPHERES

Ch/Model		Atmosphere		
		SAW	MLS	TROP
ch 4	A	0.942	0.686	0.542
	G	0.931	0.691	0.552
ch 5	A	0.930	0.579	0.410
	G	0.926	0.580	0.413

A - approximate model (modified)
 G - GENLN2 line-by-line model
 SAW - subarctic winter
 MLS - mid-latitude summer
 TROP - tropical
 Ch 4 - 885-971 cm^{-1}
 Ch 5 - 800-870 cm^{-1}

TABLE 4. TRANSMITTANCE COMPUTED FOR AVHRR CHANNELS 4 AND 5 FOR IMPORTANT ABSORBERS/SCATTERERS

Ch/Model		Absorber/Scatterer					
		H ₂ O c	H ₂ O l	CO ₂	O ₃	Aerosol	Total
ch 4	A	0.925	0.972	0.988	1.000	0.968	0.860
	G	0.93	0.97	0.985	1.000	0.97	0.85
ch 5	A	0.892	0.935	1.000	1.000	0.968	0.807
	G	0.90	0.94	0.996	1.000	0.97	0.80

All values computed using the U.S. standard atmosphere.

A - approximate model (modified)

G - GENLN2 line-by-line model

c refers to continuum absorption and l refers to line absorption.

TABLE 5. TRANSMITTANCES COMPUTED WITH THE APPROXIMATE METHOD USING THE MID-LATITUDE SUMMER ATMOSPHERE

PW (g cm ⁻²)	Transmittance	
	ch 4	ch 5
1.977	0.796	0.718
2.477	0.732	0.631
2.977	0.663	0.545
3.477	0.592	0.458
3.977	0.520	0.377

PW in g cm⁻² was varied by ± 0.5 and ± 1.0 g cm⁻² relative to the nominal mid-latitude summer value of 2.977 g cm⁻² (total value from 0 to 14 km).

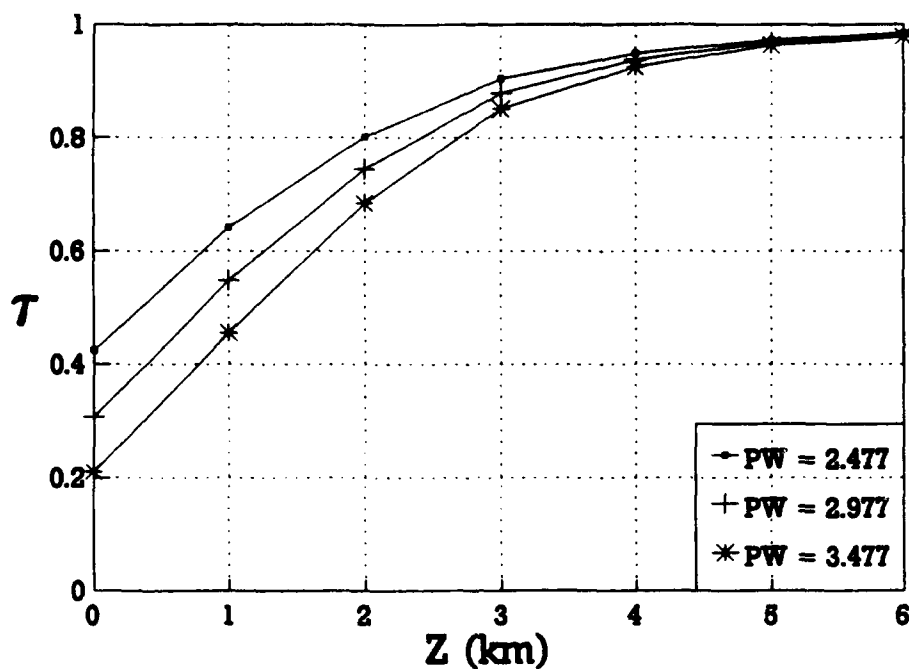


Figure 1. Transmittance (τ) values for channel 5 computed by using the approximate method for the mid-latitude summer atmosphere for 3 km horizontal paths at the indicated heights (Z) for the listed values of PW in g cm^{-2}

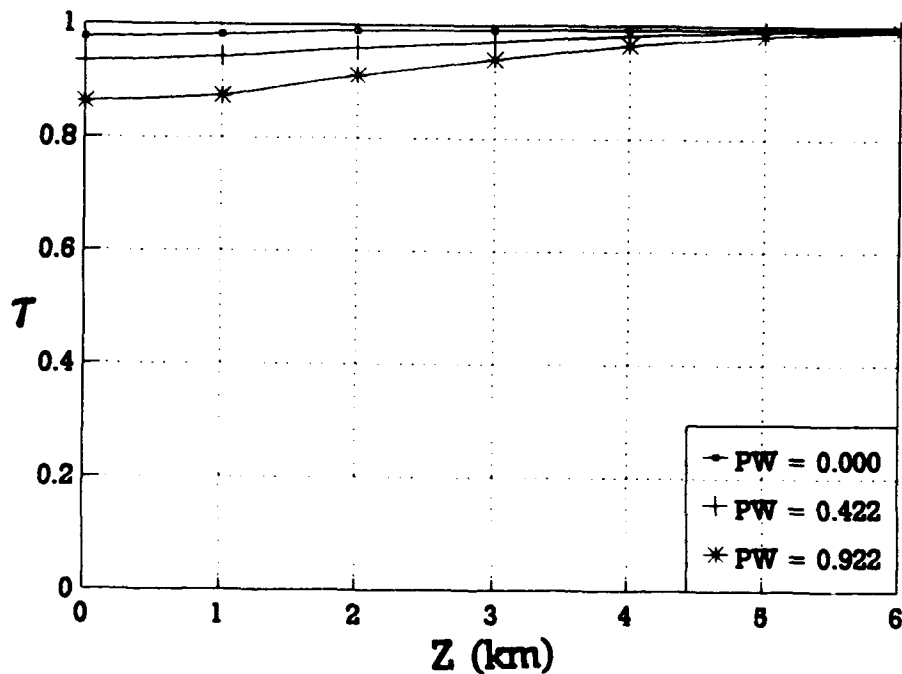


Figure 2. Transmittance (τ) values for channel 5 computed by using the approximate method for the subarctic winter atmosphere for 3 km horizontal paths at the indicated heights (Z) for the listed values of PW in g cm^{-2} .

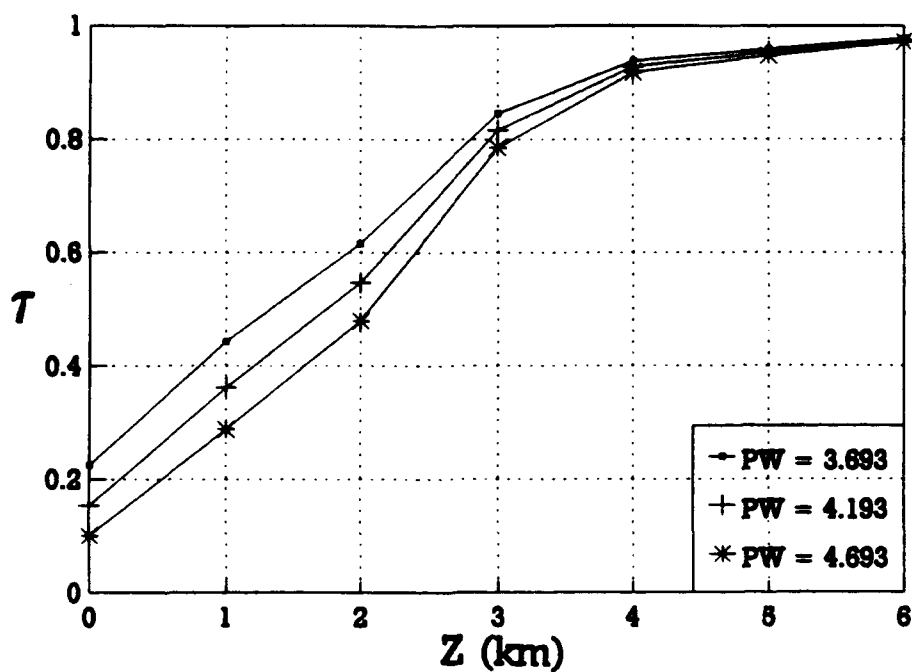


Figure 3. Transmittance (τ) values for channel 5 computed by using the approximate method for the tropical atmosphere for 3 km horizontal paths at the indicated heights (Z) for the listed values of PW in g cm^{-2} .

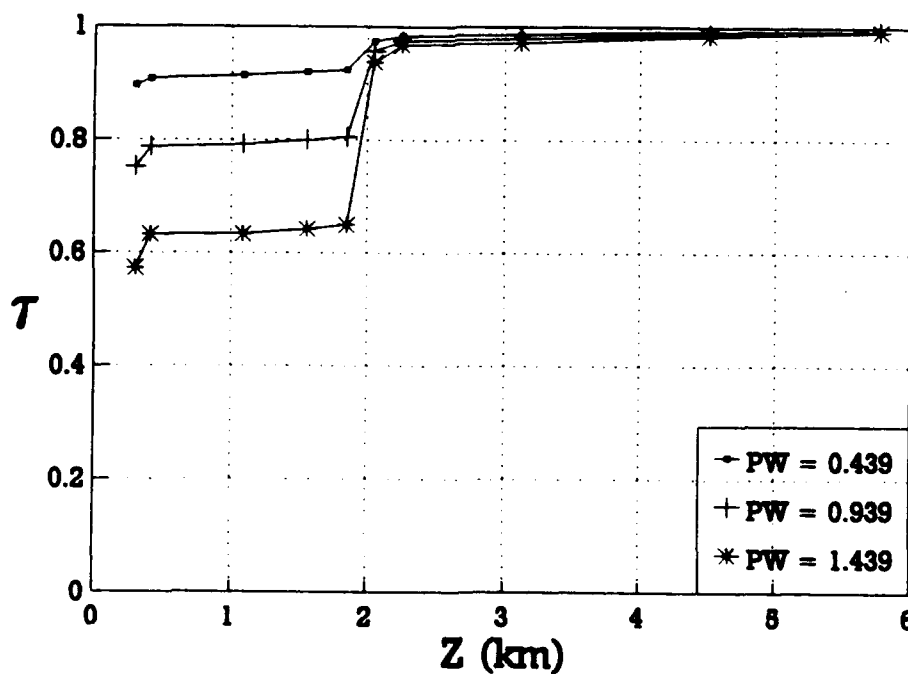


Figure 4. Transmittance (τ) values for channel 5 computed by using the approximate method for an actual sounding (see text) for 3 km horizontal paths at the indicated heights (Z) for the listed values of PW in g cm^{-2} .

LITERATURE CITED

- Bradford, G. R., B. P. Sanford, J. R. Stearns, J. A. Conant, and J. Schroeder, 1982: Airborne Background Measurements in Support of Tactical Decision Aid Development, AFGL-TR-82-0358, Geophysics Directorate, Phillips Laboratory, Hanscom AFB, MA.
- Chedin, A., H. Fischer, K. Kunzi, D. Spankuch, and N. A. Scott, 1988: Report on the ITRA Campaign and Workshop, University of Maryland, 12-14 March 1986, College Park, MD.
- Chesters, D., W. D. Robinson, and L. W. Uccellini, 1987: "Optimized Retrievals of Precipitable Water from the VAS 'Split Window'," J Clim Appl Meteorol, 1059-1066.
- Chesters, D., L. W. Uccellini, and W. D. Robinson, 1983: "Low-Level Water Vapor Fields from the VISSR Atmospheric Sounder (VAS) 'Split Window' Channels," J Clim Appl Meteorol, 725-743.
- Cogan, J., 1990: "A Method for Obtaining Remote Area Meteorological Soundings in Near Real Time," Preprints of the Fifth Conference on Satellite Meteorology and Oceanography, London, England, published by the American Meteorological Society, Boston, MA, 98-103.
- Heaps, M. G., 1982: A Vertical Structure Algorithm for Low Visibility/Low Stratus Conditions, ASL-TR-0111, U.S. Army Atmospheric Sciences Laboratory, White Sands Missile Range, NM, 38 pp.
- Jedlovac, G. J., 1990: "Precipitable Water Estimation from High Resolution Split Window Radiance Measurements," J Appl Meteorol, 863-877.
- Kleespies, T. J., and L. M. McMillin, 1990: "Retrieval of Precipitable Water from Observations in the Split Window over Varying Surface Temperatures," J Appl Meteorol, 851-862.
- Kneizys, F. X., E. P. Shettle, L. W. Abreu, J. T. Chetwynd, G. P. Anderson, W. O. Gallery, J. E. A. Selby, and S. A. Clough, 1988: Users Guide to LOWTRAN 7, AFGL-TR-88-0177, Geophysics Directorate, Phillips Laboratory, Hanscom AFB, MA.
- Kneizys, F. X., E. P. Shettle, W. O. Gallery, J. T. Chetwynd, L. W. Abreu, J. E. A. Selby, and S. A. Clough, and R. W. Fenn, 1983: Atmospheric Transmittance/Radiance: Computer Code LOWTRAN 5, AFGL-TR-83-0187, Geophysics Directorate, Phillips Laboratory, Hanscom AFB, MA.
- Kneizys, F. X., E. P. Shettle, W. O. Gallery, J. T. Chetwynd, L. W. Abreu, J. E. Selby, R. W. Fenn, and R. A. McClatchey, 1980: Atmospheric Transmittance/Radiance: Computer Code LOWTRAN 5, AFGL-TR-80-0067, Geophysics Directorate, Phillips Laboratory, Hanscom AFB, MA.

- Ludlam, F. H., 1980: Clouds and Storms: The Behavior and Effect of Water in the Atmosphere, The Pennsylvania State University Press, University Park, PA.
- McClatchey, R. A., R. W. Fenn, J. E. A. Selby, F. E. Volz, and J. S. Garing, 1972: Optical [sic] Properties of the Atmosphere (Third Edition), AFCRL-72-0497, Air Force Cambridge Research Laboratories, L. G. Hanscom Field, Bedford, MA.
- Saunders, R. W., and D. P. Edwards, 1989: "Atmospheric Transmittances for the AVHRR Channels," Appl Opt, 4154-4160.

DISTRIBUTION LIST FOR PUBLIC RELEASE

Commandant
U.S. Army Chemical School
ATTN: ATZN-CM-CC (S. Barnes)
Fort McClellan, AL 36205-5020

Commander
U.S. Army Aviation Center
ATTN: ATZQ-D-MA
Mr. Oliver N. Heath
Fort Rucker, AL 36362

Commander
U.S. Army Aviation Center
ATTN: ATZQ-D-MS (Mr. Donald Wagner)
Fort Rucker, AL 36362

NASA/Marshall Space Flight Center
Deputy Director
Space Science Laboratory
Atmospheric Sciences Division
ATTN: E501 (Dr. George H. Fichtl)
Huntsville, AL 35802

NASA/Marshall Space Flight Center
Atmospheric Sciences Division
ATTN: Code ED-41
Huntsville, AL 35812

Deputy Commander
U.S. Army Strategic Defense Command
ATTN: CSSD-SL-L
Dr. Julius Q. Lilly
P.O. Box 1500
Huntsville, AL 35807-3801

Commander
U.S. Army Missile Command
ATTN: AMSMI-RD-AC-AD
Donald R. Peterson
Redstone Arsenal, AL 35898-5242

Commander
U.S. Army Missile Command
ATTN: AMSMI-RD-AS-SS
Huey F. Anderson
Redstone Arsenal, AL 35898-5253

Commander
U.S. Army Missile Command
ATTN: AMSMI-RD-AS-SS
B. Williams
Redstone Arsenal, AL 35898-5253

Commander
U.S. Army Missile Command
ATTN: AMSMI-RD-DE-SE
Gordon Lill, Jr.
Redstone Arsenal, AL 35898-5245

Commander
U.S. Army Missile Command
Redstone Scientific Information
Center
ATTN: AMSMI-RD-CS-R/Documents
Redstone, Arsenal, AL 35898-5241

Commander
U.S. Army Intelligence Center
and Fort Huachuca
ATTN: ATSI-CDC-C (Mr. Colanto)
Fort Huachuca, AZ 85613-7000

Northrup Corporation
Electronics Systems Division
ATTN: Dr. Richard D. Tooley
2301 West 120th Street, Box 5032
Hawthorne, CA 90251-5032

Commander - Code 3331
Naval Weapons Center
ATTN: Dr. Alexis Shlanta
China Lake, CA 93555

Commander
Pacific Missile Test Center
Geophysics Division
ATTN: Code 3250 (Terry E. Battalino)
Point Mugu, CA 93042-5000

Lockheed Missiles & Space Co., Inc.
Kenneth R. Hardy
Org/91-01 B/255
3251 Hanover Street
Palo Alto, CA 94304-1191

Commander
Naval Ocean Systems Center
ATTN: Code 54 (Dr. Juergen Richter)
San Diego, CA 92152-5000

Meteorologist in Charge
Kwajalein Missile Range
P.O. Box 67
APO San Francisco, CA 96555

U.S. Department of Commerce
Mountain Administration Support
Center
Library, R-51 Technical Reports
325 S. Broadway
Boulder, CO 80303

Dr. Hans J. Liebe
NTIA/ITS S 3
325 S. Broadway
Boulder, CO 80303

NCAR Library Serials
National Center for Atmos Rsch
P.O. Box 3000
Boulder, CO 80307-3000

Bureau of Reclamation
ATTN: D: 1200
P.O. Box 25007
Denver, CO 80225

HQDA
ATTN: DAMI-POI
Washingtng, D.C. 20310-1067

Mil Asst for Env Sci Ofc of
The Undersecretary of Defense
for Rsch & Engr/R&AT/E&LS
Pentagon - Room 3D129
Washington, D.C. 20301-3080

Director
Naval Research Laboratory
ATTN: Code 4110
Dr. Lothar H. Ruhnke
Washington, D.C. 20375-5000

HQDA
DEAN-RMD/Dr. Gomez
Washington, D.C. 20314

Director
Division of Atmospheric Science
National Science Foundation
ATTN: Dr. Eugene W. Bierly
1800 G. Street, N.W.
Washington, D.C. 20550

Commander
Space & Naval Warfare System Command
ATTN: PMW-145-1G (LT Painter)
Washington, D.C. 20362-5100

Commandant
U.S. Army Infantry
ATTN: ATSH-CD-CS-OR
Dr. E. Dutoit
Fort Benning, GA 30905-5090

USAFETAC/DNE
Scott AFB, IL 62225

Air Weather Service
Technical Library - FL4414
Scott AFB, IL 62225-5458

HQ AWS/DOO
Scott AFB, IL 62225-5008

USAFETAC/DNE
ATTN: Mr. Charles Glauber
Scott AFB, IL 62225-5008

Commander
U.S. Army Combined Arms Combat
ATTN: ATZL-CAW (LTC A. Kyle)
Fort Leavenworth, KS 66027-5300

Commander
U.S. Army Combined Arms Combat
ATTN: ATZL-CDB-A (Mr. Annett)
Fort Leavenworth, KS 66027-5300

Commander
U.S. Army Space Institute
ATTN: ATZI-SI (Maj Koepsell)
Fort Leavenworth, KS 66027-5300

Commander
U.S. Army Space Institute
ATTN: ATZL-SI-D
Fort Leavenworth, KS 66027-7300

Commander
Phillips Lab
ATTN: PL/LYP (Mr. Chisholm)
Hanscom AFB, MA 01731-5000

Director
Atmospheric Sciences Division
Geophysics Directorate
Phillips Lab
ATTN: Dr. Robert A. McClatchey
Hanscom AFB, MA 01731-5000

Raytheon Company
Dr. Charles M. Sonnenschein
Equipment Division
528 Boston Post Road
Sudbury, MA 01776
Mail Stop 1K9

Director
U.S. Army Materiel Systems
Analysis Activity
ATTN: AMXSY-MP (H. Cohen)
APG, MD 21005-5071

Commander
U.S. Army Chemical Rsch,
Dev & Engr Center
ATTN: SMCCR-OPA (Ronald Pennsyle)
APG, MD 21010-5423

Commander
U.S. Army Chemical Rsch,
Dev & Engr Center
ATTN: SMCCR-RS (Mr. Joseph Vervier)
APG, MD 21010-5423

Commander
U.S. Army Chemical Rsch,
Dev & Engr Center
ATTN: SMCCR-MUC (Mr. A. Van De Wal)
APG, MD 21010-5423

Director
U.S. Army Materiel Systems
Analysis Activity
ATTN: AMXSY-AT (Mr. Fred Campbell)
APG, MD 21005-5071

Director
U.S. Army Materiel Systems
Analysis Activity
ATTN: AMXSY-CR (Robert N. Marchetti)
APG, MD 21005-5071

Director
U.S. Army Materiel Systems
Analysis Activity
ATTN: AMXSY-CS (Mr. Brad W. Bradley)
APG, MD 21005-5071

Commander
U.S. Army Laboratory Command
ATTN: AMSLC-CG
2800 Powder Mill Road
Adelphi, MD 20783-1145

Commander
Headquarters
U.S. Army Laboratory Command
ATTN: AMSLC-CT
2800 Powder Mill Road
Adelphi, MD 20783-1145

Commander
Harry Diamond Laboratories
ATTN: SLCIS-CO
2800 Powder Mill Road
Adelphi, MD 20783-1197

Director
Harry Diamond Laboratories
ATTN: SLCHD-ST-SP
Dr. Z.G. Sztankay
Adelphi, MD 20783-1197

National Security Agency
ATTN: W21 (Dr. Longbothum)
9800 Savage Road
Ft George G. Meade, MD 20755-6000

U. S. Army Space Technology
and Research Office
ATTN: Brenda Brathwaite
5321 Riggs Road
Gaithersburg, MD 20882

OIC-NAVSWC
Technical Library (Code E-232)
Silver Springs, MD 20903-5000

The Environmental Research
Institute of MI
ATTN: IRIA Library
P.O. Box 8618
Ann Arbor, MI 48107-8618

Commander
U.S. Army Research Office
ATTN: DRXRO-GS (Dr. W.A. Flood)
P.O. Box 12211
Research Trianagle Park, NC 27709

Dr. Jerry Davis
North Carolina State University
Department of Marine, Earth, &
Atmospheric Sciences
P.O. Box 8208
Raleigh, NC 27650-8208

Commander
U. S. Army CECRL
ATTN: CECRL-RG (Dr. H. S. Boyne)
Hanover, NH 03755-1290

Commanding Officer
U.S. Army ARDEC
ATTN: SMCAR-IMI-I, Bldg 59
Dover, NJ 07806-5000

U.S. Army Communications-Electronics
Command Center for EW/RSTA
ATTN: AMSEL-RD-EW-SP
Fort Monmouth, NJ 07703-5303

Commander
U.S. Army Communications-Electronics
Command
ATTN: AMSEL-EW-D (File Copy)
Fort Monmouth, NJ 07703-5303

Headquarters
U.S. Army Communications-Electronics
Command
ATTN: AMSEL-EW-MD
Fort Monmouth, NJ 07703-5303

Commander
U.S. Army Satellite Comm Agency
ATTN: DRCPM-SC-3
Fort Monmouth, NJ 07703-5303

Director
EW/RSTA Center
ATTN: AMSEL-EW-DR
Fort Monmouth, NJ 07703-5303

USACECOM
Center for EW/RSTA
ATTN: AMSEL-RD-EW-SP
Fort Monmouth, NJ 07703-5303

6585th TG (AFSC)
ATTN: RX (CPT Stein)
Holloman AFB, NM 88330

Department of the Air Force
OL/A 2nd Weather Squadron (MAC)
Holloman AFB, NM 88330-5000

PL/WE
Kirtland AFB, NM 87118-6008

Director
U.S. Army TRADOC Analysis Command
ATTN: ATRC-WSS-R
White Sands Missile Range, NM 88002

Rome Laboratory
ATTN: Technical Library RL/DOVL
Griffiss AFB, NY 13441-5700

Department of the Air Force
7th Squadron
APO, NY 09403

AWS
USAREUR/AEAWX
APO, NY 09403-5000

AF Wright Aeronautical Laboratories
Avionics Laboratory
ATTN: AFWAL/AARI (Dr. V. Chimelis)
Wright-Patterson AFB, OH 45433

AFMC/DOW
Wright-Patterson AFB, OH 0334-5000

Commander
U.S. Army Field Artillery School
ATTN: ATSF-F-FD (Mr. Gullion)
Fort Sill, OK 73503-5600

Commandant
U.S. Army Field Artillery School
ATTN: ATSF-TSM-TA
Mr. Charles Taylor
Fort Sill, OK 73503-5600

Commander
Naval Air Development Center
ATTN: Al Salik (Code 5012)
Warminster, PA 18974

Commander
U.S. Army Dugway Proving Ground
ATTN: STEDP-MT-DA-M
Mr. Paul Carlson
Dugway, UT 84022

Commander
U.S. Army Dugway Proving Ground
ATTN: STEDP-MT-DA-L
Dugway, UT 84022

Commander
U.S. Army Dugway Proving Ground
ATTN: STEDP-MT-M (Mr. Bowers)
Dugway, UT 84022-5000

Defense Technical Information Center
ATTN: DTIC-FDAC
Cameron Station
Alexandria, VA 22314

Commanding Officer
U.S. Army Foreign Science &
Technology Center
ATTN: CM
220 7th Street, NE
Charlottesville, VA 22901-5396

Naval Surface Weapons Center
Code G63
Dahlgren, VA 22448-5000

Commander
U.S. Army OEC
ATTN: CSTE-EFS
Park Center IV
4501 Ford Ave
Alexandria, VA 22302-1458

Commander and Director
U.S. Army Corps of Engineers
Engineer Topographics Laboratory
ATTN: ETL-GS-LB
Fort Belvoir, VA 22060

TAC/DOWP
Langley AFB, VA 23665-5524

U.S. Army Topo Engineering Center
ATTN: CETEC-ZC
Fort Belvoir, VA 22060-5546

Commander
Logistics Center
ATTN: ATCL-CE
Fort Lee, VA 23801-6000

Commander
USATRADO
ATTN: ATCD-FA
Fort Monroe, VA 23651-5170

Science and Technology
101 Research Drive
Hampton, VA 23666-1340

Commander
U.S. Army Nuclear & Cml Agency
ATTN: MONA-ZB Bldg 2073
Springfield, VA 22150-3198